Vapor-Liquid Equilibria for the Ethane-Propane System

D. E. MATSCHKE and GEORGE THODOS, The Technological Institute, Northwestern University, Evanston, Ill.

PHASE BEHAVIOR of the ethane-propane system has been experimentally examined at six temperatures between 100° and 200° F. and at pressures ranging up to the critical locus (3). Price (4) reports experimental equilibria data for this system at 0° and 50° F. To provide a complete presentation, the data of Price have been included with the present study.

The experimental equipment used in this investigation has been described (5, 6, 7). The basic feature of the equipment resides in an equilibrium cell, which includes a mercury-driven piston that can be made to vary the volume of the equilibrium chamber and thereby control the pressure of the system. Because of a special sampling design, coexisting vapor and liquid microsamples were obtained, thus permitting an extensive experimental coverage from a single charge. The samples were analyzed with a mass spectrometer.

To minimize temperature gradients in the air bath surrounding the equilibrium cell, two electrically driven high-speed fans were provided, which allowed the maximum over-all temperature gradient on the cell to be held within 0.4° F. Temperatures within the cell were controlled to $\pm 0.2^{\circ}$ F. The pressure could be read to ± 2 p.s.i. The accuracy of the mass spectrograph analysis was calculated, based on the minimum reliabilities of the recorded peak values, to be within 0.005 mole fraction.

The ethane and propane used were research grade hydrocarbons supplied by the Phillips Petroleum Co. The certified purities were 99.9% for ethane and 99.99%for propane.

The equilibrium constants resulting from the experimental data were related to the pressure of the system to obtain smoothed equilibrium-constant (K) values. This was accomplished by establishing plots of log PK vs. P for each temperature, as well as plots of log K vs. log P. Both of these methods of representation have advantages from the standpoint of aligning data. The first of these methods produces curves with small slopes which tend to approach zero as the pressure approaches zero, while the second method of representation produces relationships



Figure 1. Pressure-composition diagram

with slopes approaching -1 as the pressure again approaches zero. These plots were then both applied to the alignment of the K values subsequently herein reported. This information was in turn used to adjust the experimental vapor-liquid equilibrium compositions to maintain internal consistency. These aligned results are listed in Table I and are also presented graphically in Figures 1, 2, and 3. The critical temperatures and pressures established in this study are given in Table II and also appear in Figures 1 and 2. The critical pressure locus was approved along a constant temperature path by carefully adjusting the over-all cell composition and pressure. The resulting data were then analyzed to show where the bubble point and dew point lines converged, thus establishing both the critical pressure and composition corresponding to this constant temperature, which then automatically becomes the critical temperature of this mixture.

The experimental data of Price (4), which were limited to 0° and 50° F., are presented in Table III and are also included in Figures 1, 2, 3. Using the smoothing technique already outlined, the values presented in Table I were obtained and were used to produce the dashed curves of Figures 1 and 3. These curves do not necessarily pass through all the data points of Price. In Tables I and III, the vapor pressures of ethane were obtained from the work of Barkelew, Valentine, and Hurd (1); the vapor pressure data for propane were procured from the work of Stearns and George (8). The pure component critical temperatures and pressures presented in Table II were obtained from the compilation of Lydersen, Greenkorn, and Hougen (2).

For the total of approximately 70 sets of equilibrium data, the K values calculated from the experimental results showed an average deviation of 1.0% from the corresponding smoothed K's; 10% of these equilibrium constants exhibited deviations in excess of 3%, with a maximum of 9.8%. Similarly, the average deviation of the experimental equilibrium compositions was found to be 0.003



Figure 2. Temperature-composition diagram

Pressure.	Ethane, Mole Fraction		K		Pressure	Ethane, Mole Fraction		K	
P.S.I.A.	x_2	y_2	Ethane	Propane	P.S.I.A.	$\overline{x_2}$	<i>y</i> ₂	Ethane	Propane
		100° F					160° F.		
188 7ª	0	0	2.66	1.00	385.0°	0	0	1 97	1.00
200	0 0313	0 0789	2.00	0.951	400	0 0253	0 0480	1 90	0.977
250	0 149	0.310	2.02	0.811	450	0 104	0.176	1.00	0.920
300	0.255	0.455	1 79	0.732	500	0.174	0.270	1.55	0.820
350	0.353	0.558	1.75	0.683	550	0.241	0.343	1.00	0.866
400	0 447	0.638	1 43	0.655	600	0.305	0 403	1.32	0.859
450	0.535	0 704	1.32	0.636	650	0.369	0.457	1 24	0.861
500	0.622	0.764	1 23	0.625	700	0.432	0.502	1 16	0.877
550	0.705	0.816	1 16	0.624	725	0.463	0.516	1 11	0.011
600	0.781	0.861	1 10	0.625	738 0	0.400	0.506	1.00	1 000
650	0.843	0.894	1.10	0.672	100.0	0.000	0.000	1.00	1.000
700	0.895	0.004	1.00	0.739			180° F.		
725	0.919	0.935	1.00	0.825	473 2ª	0	0	1 69	1.00
731.5	0.935	0.935	1.00	1.000	500	0 0356	0 0570	1.60	0.978
101.0	0.000	0.000	1.00	1.000	525	0.0693	0.106	1.53	0.961
		120° F.			550	0.0000	0.149	1.00	0.948
243 4°	0	0	2.36	1.00	575	0 135	0 188	1 39	0.939
250	0.0130	0.0300	2.31	0.983	600	0.168	0.225	1.34	0.931
300	0.116	0.230	1.98	0.871	625	0.201	0.262	1.30	0.924
350	0.209	0.366	1 75	0.802	650	0 235	0 294	1.25	0.923
400	0.297	0.468	1.58	0.757	675	0.270	0.324	1.20	0.926
450	0.379	0.548	1.60	0.728	700	0.309	0.331	1.07	0.968
500	0.457	0.614	1 34	0 711	705.0^{b}	0.3215	0.3215	1.00	1 000
550	0.533	0.672	1.26	0.702		0.0110	0001 D	1.00	1.000
600	0.607	0.726	1.20	0.697			200° F.		
650	0.678	0.773	1.14	0.706	575.0ª	0	0	1.47	1.00
700	0.745	0.815	1.09	0 727	580	0.0065	0.0095	1 46	0.997
725	0.773	0.826	1.07	0.767	590	0.0193	0.0275	1 42	0.992
750	0.801	0.821	1.025	0.899	600	0.0320	0.0446	1 39	0.987
752.0	0.810	0.810	1.00	1.000	610	0.0445	0.0602	1.35	0.983
	*****	10.5	2.00	21000	620	0.0566	0.0742	1.31	0.981
		140° F.			630	0.0682	0.0869	1.27	0.980
308.4°	0	0	2.21	1.00	640	0.0791	0.0949	1.20	0.983
350	0.0711	0.140	1.97	0.926	645	0.0846	0.0953	1.13	0.988
400	0.152	0.267	1.76	0.864	648.4°	0.0930	0.0930	1.00	1.000
450	0.230	0.367	1.60	0.822		т			
500	0.305	0.448	1.47	0.794		1	Jata of Price (4	F)	
550	0.378	0.515	1.36	0.780			0° F.		
600	0.448	0.573	1.28	0.774	07.04	0	0	F 07	1.00
650	0.515	0.618	1.20	0.788	37.8	0 0705	0 004	5.07	1.00
700	0.581	0.655	1.13	0.823	00	0.0785	0.304	3.87	0.755
725	0.613	0.672	1.10	0.848	100	0.373	0.743	1.99	0.410
750	0.652	0.670	1.03	0.947	100	0.040	0.891	1.38	0.308
752.0°	0.6685	0.6685	1.00	1.000	200	1,000	0.972	1.08	0.287
					219.7	1.000	1.000	1.00	1.00
							50° F.		
					91.5°	٥	0	3 69	1.00

Table L. Smoothed Equilibrium Compositions and Equilibrium Constants

mole fraction from the corresponding smoothed values. Again, 10% of these equilibrium compositions were found to deviate in excess of 0.010 mole fraction, with a maximum deviation of 0.027 mole fraction.

The majority of the deviations fall within the expected uncertainty of the mass spectrograph analyses. The larger deviations were primarily encountered at low pressures, where the uncertainty in their measurement contributes signifcantly in producing these deviations. For pressures near the critical point, slow equilibrium responses contributed to an occasional deviation of significance.

Ethane Mole Fraction	Critical Temp., ° R.	Critical Pressure, P.S.I.A
0ª	665.8	617.4
0.10	659.5	651
0.20	651.5	678
0.30	642.2	701
0.40	632.0	721
0.50	620.8	737
0.60	608.7	748
0.70	595.6	753
0.80	581.3	753
0.90	565.6	741
1.00^{a}	549.7	708.5

575.0 ^a 580 590 600 610 620 630 640	$\begin{array}{c} 0\\ 0.0065\\ 0.0193\\ 0.0320\\ 0.0445\\ 0.0566\\ 0.0682\\ 0.0791\\ 0.0791\end{array}$	0 0.0095 0.0275 0.0446 0.0602 0.0742 0.0869 0.0949	$1.47 \\ 1.46 \\ 1.42 \\ 1.39 \\ 1.35 \\ 1.31 \\ 1.27 \\ 1.20 \\ $	$1.00 \\ 0.997 \\ 0.992 \\ 0.983 \\ 0.981 \\ 0.980 \\ 0.983 \\ 0.983 \\ 0.980 \\ 0.983$			
648.4°	0.0930	0.0933	1.13	1.000			
	Γ	Data of Price (4	4)				
	-	0° F.	,				
37.8° 50 100 150 200 219.7 ^c	$\begin{array}{c} 0 \\ 0.0785 \\ 0.373 \\ 0.646 \\ 0.901 \\ 1.000 \end{array}$	0 0.304 0.743 0.891 0.972 1.000	5.07 3.87 1.99 1.38 1.08 1.00	$1.00 \\ 0.755 \\ 0.410 \\ 0.308 \\ 0.287 \\ 1.00$			
50° F.							
91.5° 100 150 200 250 300 350 400 437.5°	$\begin{matrix} 0 \\ 0.031 \\ 0.195 \\ 0.357 \\ 0.507 \\ 0.651 \\ 0.781 \\ 0.911 \\ 1.000 \end{matrix}$	$\begin{array}{c} 0 \\ 0.104 \\ 0.454 \\ 0.646 \\ 0.763 \\ 0.848 \\ 0.905 \\ 0.961 \\ 1.000 \end{array}$	3.62 3.34 2.33 1.81 1.50 1.30 1.16 1.06 1.00	$1.00 \\ 0.925 \\ 0.678 \\ 0.550 \\ 0.480 \\ 0.434 \\ 0.430 \\ 0.442 \\ 1.000$			

^a Vapor pressure of propane (8). ^b Critical point. ^c Vapor pressure of ethane (1).

Table III. Experimental Equilibrium Data of Price (4) for Ethane-Propane System at 0° and 50° F.

-	mane i repai	ie eystenn ar e		•	
Pressure.	Ethane, M	ole Fraction	K		
P.S.I.A.	x_2	y_2	Ethane	Propane	
		0° F.			
37.8°	0	0		1.000	
100	0.373	0.692	1.85	0.491	
200	0.9013	0.9717	1.08	0.287	
219.7^{b}	1.00	1.000	1.00	1.000	
		50° F.			
91.5°	0	0		1.000	
100	0.0236	0.0720	3.05	0.951	
200	0.357	0.612	1.72	0.603	
300	0.651	0.848	1.30	0.434	
400	0.9108	0.9606	1.05	0.442	
437.5	1.000	1.000	1.00	1.000	
^a Vapor pressu	ire of propane	(8). ^b Vapor pr	essure of eth	ane (1).	

233



Figure 3. Vapor-liquid equilibrium constants

ACKNOWLEDGMENT

The authors are grateful to the National Science Foundation for the support which made this study possible. Appreciation is also extended to T.W. Legatski of the Phillips Petroleum Co. for his interest and for the contribution of the hydrocarbons used.

LITERATURE CITED

- (1) Barkelew, C.H., Valentine, J.L., Hurd, C.O., Trans. Am. Inst. Chem. Eng. 43, 25 (1947).
- (2) Lydersen, A.L., Greenkorn, R.A., Hougen, O.A., Wisconsin Univ. Eng. Exp. Sta., Rept. 4, October 1955.
- Matschke, D.E., Ph.D. dissertation, Northwestern Univ., Evanston, Ill., 1962.
- (4) Price, A.R., Ph.D. dissertation, Rice Inst., Houston, Tex., (1957).
- (5) Rigas, T.J., Ph.D. dissertation, Northwestern Univ., Evanston, Ill., (1957).
- (6) Rigas, T.J., Mason, D.F., Thodos, George, Ind. Eng. Chem. 50, 1297 (1958).
- (7) Rigas, T.J., Mason, D.F., Thodos, George, J. CHEM. ENG. Data 4, 201 (1959).
- (8) Stearns, W.V., George, E.J., Ind. Eng. Chem. 35, 602 (1943).

RECEIVED for review October 9, 1961. Accepted December 19, 1961.

Lennard-Jones Force Constants Predicted from Critical Properties

LEONARD I. STIEL and GEORGE THODOS

The Technological Institute, Northwestern University, Evanston, III.

EQUATIONS developed by Hirschfelder, Curtiss, and Bird (4) for the calculation of the transport properties of nonpolar gases at moderate pressures have found widespread application. These equations were developed using the Lennard-Jones force potential,

$$\phi(\mathbf{r}) = 4\epsilon \left[\left(\frac{\sigma}{r} \right)^{12} - \left(\frac{\sigma}{r} \right)^{6} \right]$$
(1)

as the proper expression of the intermolecular forces between the molecules; and consequently, the equations require the Lennard-Jones force constants, ϵ/κ and σ , for the calculation of viscosity, thermal conductivity, and selfdiffusivity. These equations can be expressed as follows:

$$\mu = 2.6693 \times 10^{-5} \frac{(MT)^{1/2}}{\sigma^2 \Omega^{(2,2)*}[T_N]}$$
(2)

and

$$k = 19.891 \times 10^{-5} \frac{(T/M)^{1/2}}{\sigma^2 \Omega^{(2,2)*}[T_N]}$$
(3)

$$\Delta = 262.80 \times 10^{-5} \frac{(T^3/M)^{1/2}}{\pi \sigma^2 \Omega^{(1,1)*}[T_N]}$$
(4)

where $\Omega^{(1,1)*}[T_N]$ and $\Omega^{(2,2)*}[T_N]$ are tabulated functions of the normalized temperature, $T_N = T/(\epsilon/\kappa)$.

The Lennard-Jones force constants required in these equations can be obtained from either second virial coefficients or from viscosity data for gases. Hirschfelder, Bird, and Spotz (3) compare force constants obtained from both methods for a number of common substances. Equations 2, 3, and 4 can be applied only to those substances for which experimental P-V-T data and/or viscosities are available for the establishment of the force constants. Because of this limitation, several attempts have been made to relate the force constants of a substance to its critical properties. Bird, Stewart, and Lightfoot (1) present the following relationships between the Lennard-Jones force constants and the critical properties of a substance, which were developed from semitheoretical considerations:

$$\kappa = 0.77 T_c$$
 (5)

$$\sigma = 0.841 \, v_c^{1/3} \tag{6}$$

Flynn (2) has calculated Lennard-Jones force constants from viscosity data for 16 hydrocarbons for which reliable experimental viscosities are available, including the normal paraffins up to nonane, olefins, acetylenes, naphthenes, and aromatics. These values and those determined from viscosity data by Hirschfelder, Curtiss, and Bird (4) for 11 nonhydrocarbon substances, including the inert and diatomic gases, carbon dioxide, and carbon tetrachloride, were used to compare the Lennard Jones force constants resulting from Equations 5 and 6. The data used in these calculations are presented in Table I. An average deviation of 20.4% resulted for the temperature force constant, ϵ/κ , and 4.6% for σ , the collision diameter.

JOURNAL OF CHEMICAL AND ENGINEERING DATA

ţ